

Application of NPI Decline to Gas-injection Transient Analysis

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Abstract: According to no theory nor software for gas-injection transient analysis published yet, the equation for gas injection seepage was solved to obtain NPI decline curves for gas-injection on the basis of modified material balance time. Production data were handled by use of calculator programs in Matlab to acquire drained parameters for gas-injection through typical curves fitting, which has the feature to forecast gas-injection performance in the future using the results of gas-injection analysis eventually. Calculation of C21 well production data using the method above shows that the drainage parameters for gas-injection close to that from Well Testing, and the forecasted production performance is in line with the real injection data, which prove the method above valid in analyzing gas-injection effectively. The result above provides a new tool for gas-injection transient analysis.

Keywords: UGS; gas-injection; transient analysis; NPI decline; modified theory for gas withdraw

The peak shaving capability of underground gas storage in gas field mostly depends on numerous inject-produce wells^[1-3]. So it is very important to predict the performance of single well injection-production accurately. The analysis method of single well production gas performance mainly referring to the theory of gas reservoir development represented by NPI transient production analysis based on the principle of the transient testing and daily production data^[4-6] to solving drainage parameters by fitting production typical curve and then to forecast the future production. As an important analysis tool for gas reservoir development, this production transient

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method has been developed into commercial softwares such as FAST, RTA and Topaze^[7-8] etc. However those softwares have no feature to analyze the injection gas data. The reason mainly embodies no mathematical model has been published up to now yet. In view of the problem above, new NPI model for gas injection was established to calculate drainage parameters during gas injection by typical curve matching and form a tools for gas injection forecasting eventually.

1 Seepage equation for gas injection

Single well drainage area can be simplified into closed formation as a result of the existence of fluid boundary among gas injection wells. Now the problem is converted into solving circular closed formation with a well injecting (-Q) and the comprehensive seepage shows as equation (1):

$$\left\{ \begin{array}{l} \frac{1}{r} \frac{\partial}{\partial r} (r \frac{\partial p_m}{\partial r}) = \frac{\phi \mu c_t}{K} \frac{\partial p_m}{\partial t} \\ p_m(r, t) = p_{mi} \\ r \frac{\partial p_m}{\partial r} \Big|_{r=r_w} = \frac{Q\mu}{2\pi Kh} r \\ \frac{\partial p_m}{\partial r} \Big|_{r=r_e} = 0 \end{array} \right. \quad (1)$$

Solve the above equation (1) by dimensionless treatment and using laplace transform, and obtain the result as equation (2) shows:

$$\left\{ \begin{array}{l} \frac{d^2 \bar{p}_D}{dr_D^2} + \frac{1}{r_D} \frac{d\bar{p}_D}{dr_D} = s \bar{p}_D \\ \frac{d\bar{p}_D}{dr_D} \Big|_{r_D=1} = -\frac{1}{s} \\ \frac{d\bar{p}_D}{dr_D} \Big|_{r_D=r_{eD}} = 0 \end{array} \right. \quad (2)$$

The general solution of equation (2) is a linear combination of Bessel fuction I_0 and K_0 :

$$\bar{p}_D = A_0 I_0(r_D \sqrt{s}) + B_0 K_0(r_D \sqrt{s}) \quad (3)$$

Put in the definite conditions and obtain the expression of A0 and B0, then get

the expression of pressure for gas injection as equation (4) below. Pressure for gas injection shows the same expression as that for gas withdrawing with different parameters meaning.

$$\bar{p}_D = \frac{K_1(r_{eD}\sqrt{\beta s})I_0(r_D\sqrt{\beta s}) + I_1(r_{eD}\sqrt{\beta s})K_0(r_D\sqrt{\beta s})}{s\sqrt{s}(K_1(\sqrt{\beta s})I_1(r_{eD}\sqrt{\beta s}) - I_1(\sqrt{\beta s})K_1(r_{eD}\sqrt{\beta s}))} \quad (4)$$

Dimensionless pressure p_D shows as (5):

$$p_D = \frac{2\pi Kh(p_{wf} - p_i)}{q\mu B} \quad (5)$$

Dimensionless time t_{DA} shows as (6):

$$t_{DA} = \frac{Kt}{\pi\phi\mu c_i r_e^2} \quad (6)$$

$$\beta = \frac{1}{\pi(r_e^2 - 1)} \quad (7)$$

Dimensionless radius r_D and r_{eD} shows as (8) and (9):

$$r_D = \frac{r}{r_w} \quad (8)$$

$$r_{eD} = \frac{r_e}{r_w} \quad (9)$$

2 Typical curve for gas injection

2.1 Theoretical curve

Use Stefest^[9-10] method to numerical inversion of equation (4) to get real space P_{Dd} and t_{ca}/d , then draw the curve of P_{Dd} and t_{ca}/d as shown in figure 1, which shows the same chart form as gas withdraw just with different meanings of P_{Dd} and t_{ca}/d .

2.2 Actual curve

① Calculation of material balance time. A simplified method for calculation of material balance time was provided, firstly take viscosity and compressibility with the

bottomhole flowing pressure correspondingly, then use numerical integration method, and calculate the material balance time eventually by equation (10):

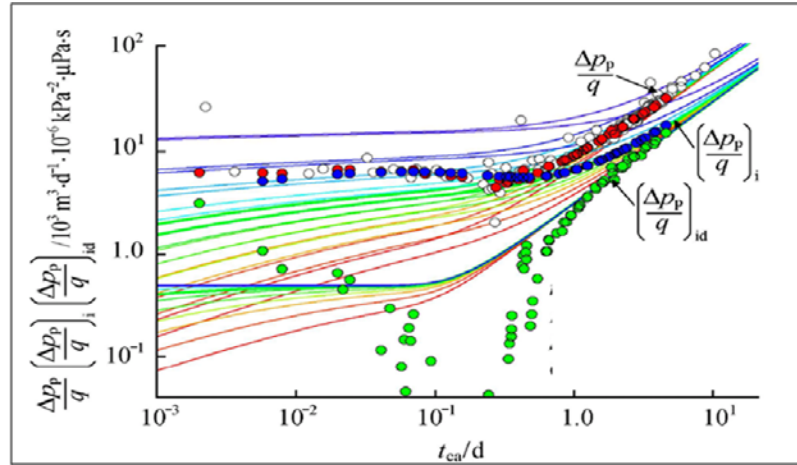


Figure 1 NPI curve of P_{Dd} and t_{ca}/d for gas injection

$$t_{ca} = \frac{(\mu c_t)_i}{q} \int_0^t \frac{q}{\mu c_t} dt \quad (10)$$

② Calculation of normalized pressure. Calculate normalized pressure according to Lee and Holditch's pseudo pressure expression and equation (12):

$$p_p = \left(\frac{\mu Z}{p}\right)_i \int_0^p \frac{p}{\mu Z} dp \quad (11)$$

$$\frac{\Delta p_p}{q} = \frac{P_{p_{wf}} - P_{p_i}}{q} \quad (12)$$

③ Drawing curve with material balance time and normalized pressure obtained from the results of ② and ① above.

3 Drainage parameters solving

Calculate material balance time and normalized pressure for each production point correspondingly. And then draw double logarithmic scatter diagram between $\Delta p_p / q - t_{ca}$ as shown in Figure 1 to solve parameters by theoretical curve and

scatter diagram matching.

① Calculate the dimensionless radius of well drainage r_{eD} by picking up one fitting point according to the results of fitting diagram.

② Calculate the permeability of injection well drainage area K by picking up the theoretical fitting point $(t_{caDA}, P_D)_M$ and actual fitting point $(t_{ca}, \Delta p_p / q - t_{ca})_M$.

$$K = \frac{(p_D)_M \mu B}{(\Delta P_p / q)_M 2\pi h} \quad (13)$$

③ Calculate the injection well drainage radius r_e by the results of steps ② above.

$$r_e = \sqrt{\frac{K}{\pi \phi \mu c_t} \left(\frac{t_{ca}}{t_{caDA}} \right)_M} \quad (14)$$

④ Calculate the injection well drainage effective radius r_{wa} by the results of steps ② and steps ③ above.

$$r_{wa} = \frac{r_e}{r_{eD}} \quad (15)$$

⑤ Calculate the injection well skin s by the results of steps ③ and steps ④ above.

$$s = \ln\left(\frac{r_w}{r_{wa}}\right) \quad (16)$$

⑥ Put above parameters obtained from steps ①②③④⑤ into the in seepage equation in order to realize the dynamic performance forecasting of gas injection.

4 Example

Take C21 well of some UGS in China's circum-Bohai-Sea area for example, the net pay is 6.8m, porosity is 0.189, irreducible water saturation is 0.65, radius of well is 0.107m, formation temperature is 358 K and relative density of gas is 0.66. The well head pressure of C21 well increased from 17 MPa to 26 MPa after continuous

gas injection for 74 days. Solve the drainage parameters through typecurve fitting method mentioned above, and acquire the result shown as Table 1.

Table 1 Drainage parameters obtained from NPI and Well-test

Methods	Permeability (mD)	Drainage Radius (m)
NPI	19.8	327
Well-test	21.2	341

It shows that the value of drainage parameters obtained from NPI method above close to that from well test, such as the two permeabilities are 19.8 mD and 21.2 mD, and the drainage area radiuses are 327 mD and 341 mD, which increases confidence in the injection NPI method.

Put the drainage parameters into seepage equation and get the prediction model for gas injection. Forecast the flowing downhole pressure based on the injection rates, then compare with actual operation of bottomhole pressure correspondingly, therefore get the history matching results shown in Figure 2 Eventually. Comparison results show that the theoretical predictions close to the actual operation result within the scope of permissible error 5%.

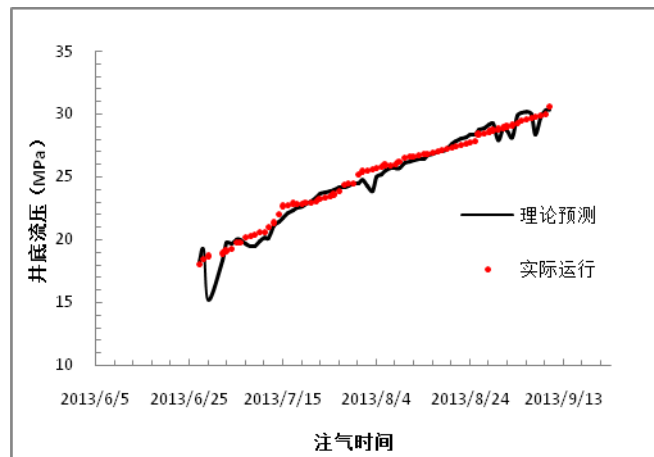


Figure 2 History matching of well head pressure by NPI method

5 Conclusion

(1) Obtain the expression of pressure for gas injection in NPI formation by modification of material balance time and pseudo-pressure.

(2) Get the NPI typical curve for gas injection by fitting theoretical curve and actual curve with the same expression as that of gas withdrawing but not the different meaning of parameters.

(3) Case study shows that the drainage parameters of injection well obtained by picking up the theoretical fitting point and actual fitting point close to that from well test, which increase confidence in NPI method for gas injection.

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